

## CLAIMS:

1. An integrated tuner circuit, comprising:
  - a tuned LC band-pass filter (10) having a variable capacitance ( $C_t$ ) and fixed inductance (L);
  - an external load capacitor having a variable capacitance ( $C_t$ ); and
  - a fixed-frequency control loop (30) for producing a voltage ( $V_{TUN}$ ) for adjusting the variable capacitances of the band-pass filter and external load capacitor to achieve tracking of the band-pass filter with an arbitrary oscillator frequency  $\omega_{LO}$ .
2. The integrated tuner circuit according to claim 1, wherein the fixed-frequency control loop (30) further comprises a fixed-frequency oscillator (32) and a circuit (34) for receiving a programmable value N for setting the value of  $\omega_{LO}$ , wherein the fixed-frequency control loop adjusts the variable capacitances  $C_t$  such that  $C_t \propto (\omega_{LO} \pm \omega_{IF})^{-2} \propto N^{-2}$ , wherein  $\omega_{IF}$  is an intermediate frequency.
3. The integrated tuner circuit according to claim 2, wherein the band-pass filter (10) is tuned to each of a plurality of different IF distances from  $\omega_{LO}$  by adjusting the programmable value N.
4. The integrated tuner circuit according to claim 2, wherein the fixed-frequency oscillator (32) outputs a signal having a frequency  $\omega_{xtal}$ , and wherein the tuned LC band-pass filter (10) is tuned to a virtual oscillator frequency  $\omega_{LO}$  given by  $N\omega_{xtal}$ .
5. The integrated tuner circuit according to claim 1, wherein the fixed-frequency control loop (30) provides compensation for parasitic capacitance ( $C_p$ ).
6. The integrated tuner circuit according to claim 5, further comprising a capacitor corresponding to the parasitic capacitance  $C_p$  in parallel with the external load capacitor.

7. The integrated tuner circuit according to claim 1, wherein the fixed-frequency control loop (30) operates to produce a signal:

$$1 - (\alpha \omega_{\text{xtal}}^2 R^2 C) N^2 C_t \rightarrow 0$$

where  $\alpha$  is a variable gain,  $\omega_{\text{xtal}}$  is a frequency of a fixed-frequency oscillator, R is a resistance, C is a capacitance, and N is a programmable value for setting the value of  $\omega_{\text{LO}}$ .

8. The integrated tuner circuit according to claim 7, wherein N and  $C_t$  are the only oscillator frequency dependent variables.

9. A method for tracking a LC tuned band-pass filter (10) with an arbitrary oscillator  $\omega_{\text{LO}}$ , wherein the band-pass filter includes a variable capacitance  $C_t$  and a fixed inductance (L), comprising:

providing a fixed-frequency control loop (30) for producing a voltage ( $V_{\text{TUN}}$ ) for adjusting the variable capacitance  $C_t$  of the tuned band-pass filter (10) and for adjusting a variable capacitance  $C_t$  of a load capacitor; and

inputting a programmable value N into the fixed-frequency control loop (30) for setting the value of  $\omega_{\text{LO}}$ , wherein the fixed-frequency control loop adjusts the variable capacitances  $C_t$  such that  $C_t \propto (\omega_{\text{LO}} \pm \omega_{\text{IF}})^{-2} \propto N^{-2}$ , wherein  $\omega_{\text{IF}}$  is an intermediate frequency.

10. The method according to claim 9, further comprising:

tuning the band-pass filter (10) to each of a plurality of different IF distances from  $\omega_{\text{LO}}$  by adjusting the programmable value N.

11. The method according to claim 9, wherein the fixed-frequency control loop (30) includes a fixed-frequency oscillator (32) that outputs a signal having a frequency  $\omega_{\text{xtal}}$ , further comprising:

tuning the band-pass filter (10) to a virtual oscillator frequency  $\omega_{\text{LO}}$  given by  $N\omega_{\text{xtal}}$ .

12. The method according to claim 9, wherein the fixed-frequency control loop (30) provides compensation for parasitic capacitance ( $C_p$ ).

13. The method according to claim 12, further comprising:

providing a capacitor corresponding to the parasitic capacitance  $C_p$  in parallel with the load capacitor.

14. The method according to claim 9, wherein the fixed-frequency control loop (30) operates to produce a signal:

$$1 - (\alpha\omega_{\text{xtal}}^2 R^2 C) N^2 C_t \rightarrow 0$$

where  $\alpha$  is a variable gain,  $\omega_{\text{xtal}}$  is a frequency of a fixed-frequency oscillator,  $R$  is a resistance, and  $C$  is a capacitance.

15. The method according to claim 14, wherein  $N$  and  $C_t$  are the only oscillator frequency dependent variables.